Fogningsdagar - Svetskommissionens medlemsdagar

## Processoptimering av reparationssvetsning av järnvägsräls med hjälp av simulering

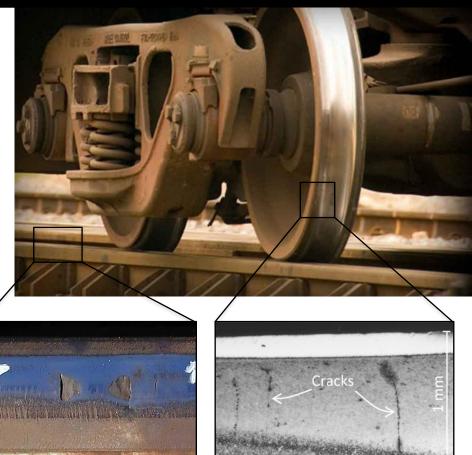
Björn Andersson, Tekn lic 2022-04-07



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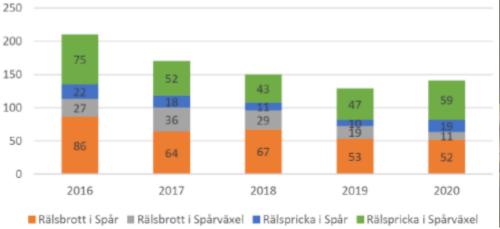
# **Background and motivation**

- High temperature railway processes:
  - Welding
  - Grinding
  - Train wheel braking (rail and wheel)
- What happens:
  - Phase transformations
  - Inhomogeneous material properties
- Practical consequences:
  - Residual stresses, interaction with operational loads
  - Initiation of cracks



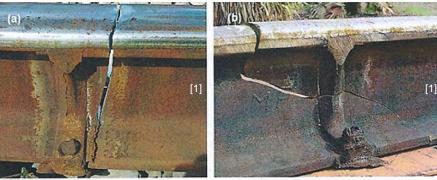
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# Rälsbrott och stora Rälsprickor i spår och spårväxel



- Decreasing number of rail fractures
- Increasing number of rail cracks
- 33-50% of the fractures in welds
- More cracks and fractures during colder periods





#### **Rail section repair - Thermite welding**





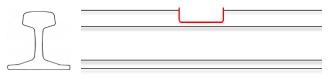
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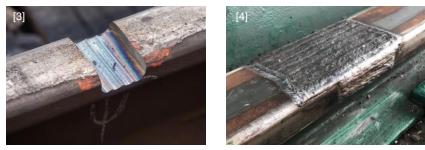
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- Remove entire damaged rail section
- Large heat input
- Slower cooling, pearlite formation, tensile residual stresses in web
- Labor intensive, time consuming

#### Rail head repair – MIG/MMA welding





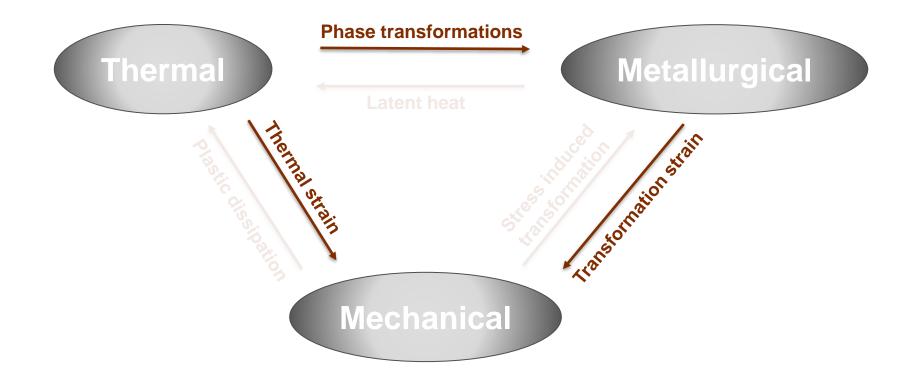
- Remove only railhead damage (or switches)
- Small, local heat input, several weld passes
- Rapid cooling, risk for martensite formation
- Quicker operation

#### New material model

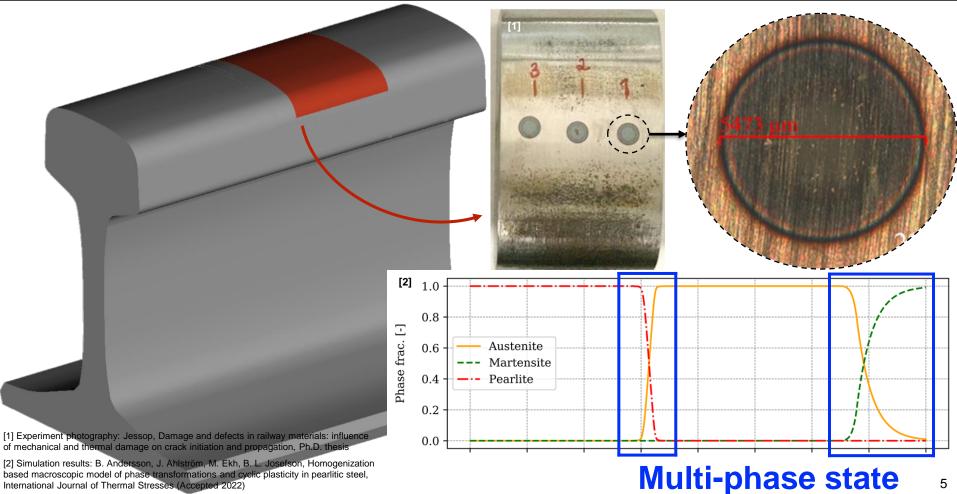
- Complex microstructure evolution
- Effects of phases and phase transformations









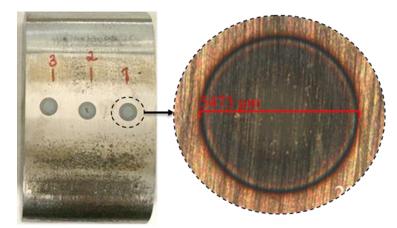


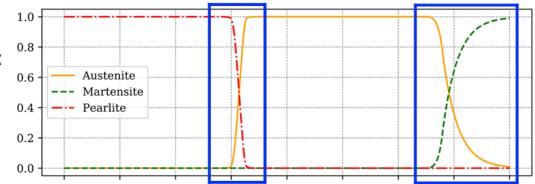
International Journal of Thermal Stresses (Accepted 2022)



Voigt assumption
$$\boldsymbol{\epsilon}_{x} = \bar{\boldsymbol{\epsilon}}$$
  
 $\bar{\boldsymbol{\sigma}} = \sum_{x} p_{x} \, \boldsymbol{\sigma}_{x}$ Reuss assumption: $\boldsymbol{\sigma}_{x} = \bar{\boldsymbol{\sigma}}$   
 $\bar{\boldsymbol{\epsilon}} = \sum_{x} p_{x} \, \boldsymbol{\epsilon}_{x}$ Self-consistent  
(Eshelby's inclusion 1957) $\bar{\boldsymbol{\sigma}} = \sum_{x=1}^{n_{x}} p_{x} \mathbf{E}_{x}^{e} : \boldsymbol{\epsilon}_{x}$ Linear mixture $\mathbf{E}^{e} = \sum_{x=1}^{n_{x}} p_{x} \mathbf{E}_{x}^{e}$  $\bar{\boldsymbol{\sigma}} = \mathbf{E}^{e} : \bar{\boldsymbol{\epsilon}}$  $\bar{\boldsymbol{\sigma}} = \mathbf{E}^{e} : \bar{\boldsymbol{\epsilon}}$ 

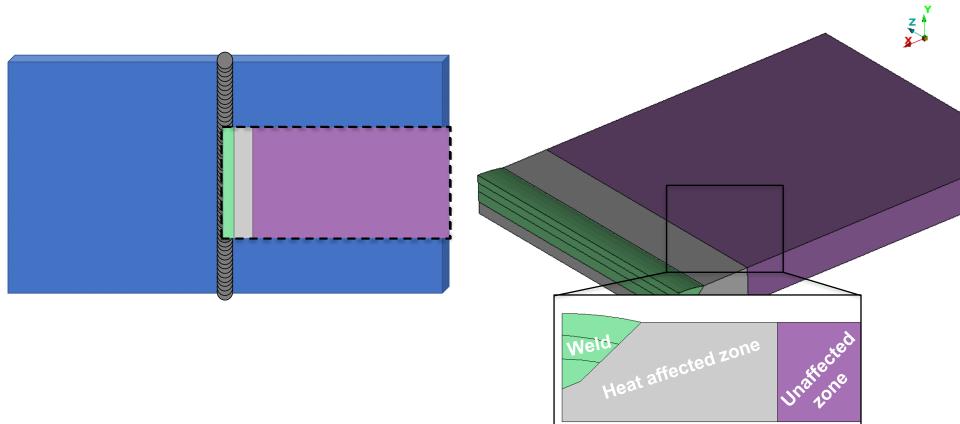
#### Homogenization methods















#### Butt welded plate - Rail head repair weld

- In principle similar
- Different geometry effects:
  - Local: Similar microstructure in weld and HAZ
  - Global: Different residual stress field
- Similar enough for simulation methodology development

## Moving heat source

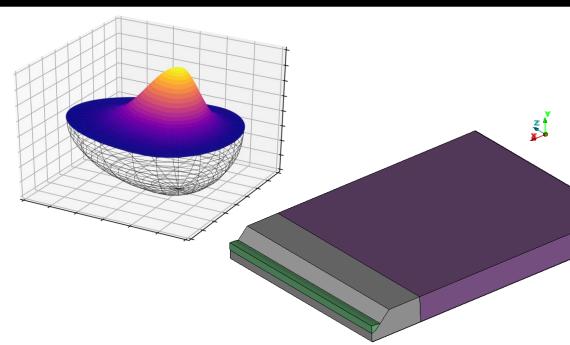
- Power input
- Weld speed
- Heat distribution (Goldak et al. 1986)

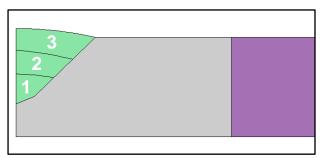
# Continuous addition of filament elements

- "Silent" elements
- Activation moving with heat source
- Material properties, zero-strain temperature

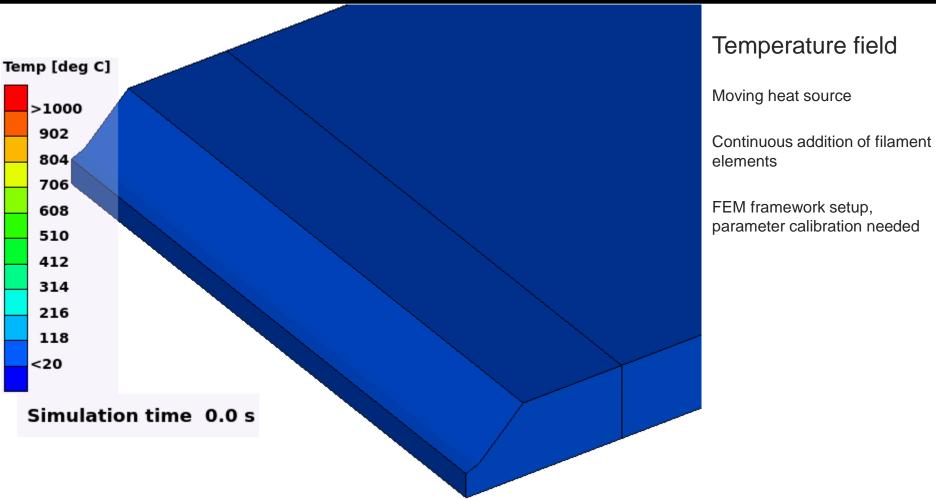
## Multiple weld passes

- Preheat, weld prep, etc.
- Cooling time between passes

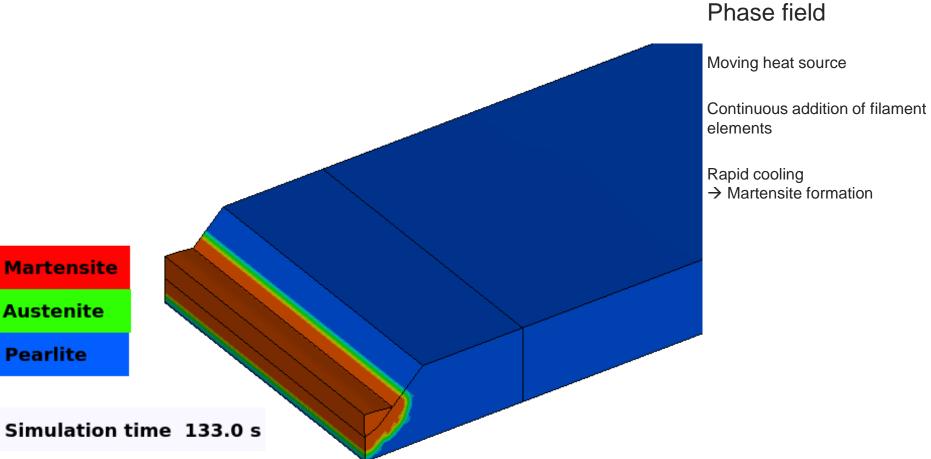




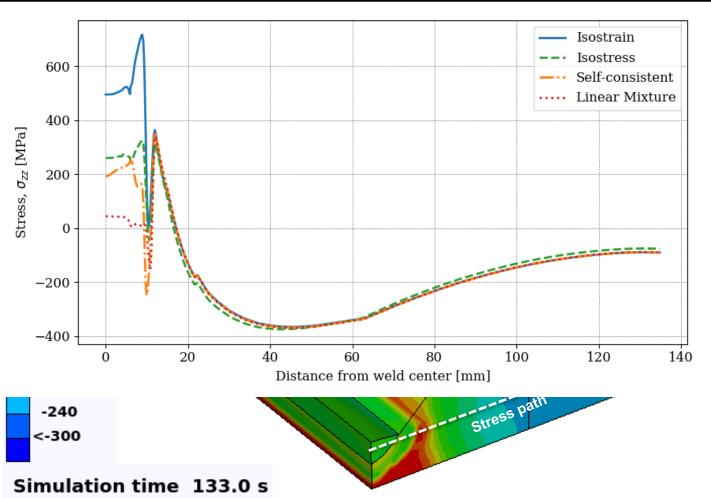








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Residual stress field Longitudinal stress

Basis for process parameter optimization together with phase evolution.

Optimization goal: Avoid both tensile stresses in certain regions and martensite formation

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# Summary and conclusions

- Thermo-mechanical-metallurgical model:
  - Phase / microstructure evolution
  - Homogenization of phase mechanical behavior
  - Transformation induced plasticity (TRIP)
  - Effect of phase transformation
- Advanced model for welding
- Comparing homogenization methods:
  - Computational time and convergence issues
  - Residual stress states in heat affected zone
- Future Work
  - Full scale simulation of repair welding process
  - Optimize process parameters and controlled pre-heating and operation temperature:
    - Avoid martensite formation
    - Avoid unfavorable residual stresses

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# Thank you

Processoptimering av reparationssvetsning av järnvägsräls med hjälp av simulering Björn Andersson abjorn@chalmers.se

CHARMEC Project MU37 – Numerical simulations of welding and other high temperature operations

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